

A Novel CPW BandPass Filter Integrating Periodic Rectangular Slot Cells

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Abstract

In this paper, we introduce the design and the achievement of a Bandpass filter structure based on the use of rectangular slot cell. The originality of this work is to achieve a coplanar filter easy to integrate with microwave planar circuits and having a wide frequency bandwidth. The proposed bandpass filter is a low cost and compact planar filter structure. The final circuit is simulated by using two electromagnetic solvers, ADS and HFSS. The validation into simulation is based on using optimization methods integrated into the both solvers. Simulations have taken into account a high meshing density to cover the whole circuit. The fabricated bandpass filter has an area of 35X31mm² and having a good insertion loss around -0.75dB in the bandwidth. The comparison between simulation and measurement results presents a good agreement.

Keywords: Cpw, Bandpass Filter, Microstrip, Periodic Structure

1. Introduction

Recently, the coplanar waveguide (CPW) technology has been widely used in the design of microwave filters, antennas and other radiofrequency circuits [1-5]. Among applications of CPW structures which can be found in literature, we have many research studies on satellite systems and mobile communications [6-13]. Therefore, the aim of this research study is to use the CPW technology in order to develop a novel CPW filter with a wide frequency band and having miniature dimensions. To do so, we have to choose the technique which will be used to design such circuit. To achieve a wide frequency bandwidth bandpass filter we can find the technique based on aperture compensation technique [14], direct frequency conversion design method [15], using stepped impedance dual-mode resonator [16], etc.

After studying the different techniques used for the achievement of wide frequency bandwidth bandpass filters. We propose in this work, a simple technique based on the use of CPW technology and in the same time the integration of a periodic structures permitting the enlargement of the frequency band. The periodic structure which was used is an optimized slot rectangular shape. The final bandpass filter is formed from a CPW centered line coupled to two lines in which we have etched the rectangular slot repeated periodically.

The following sections, will present the different steps

followed to design and to simulate the proposed bandpass filter, and at the end a comparison between simulation and measurement results.

2. Design Procedure

Firstly, we have designed a 50 Ohm CPW line matched by using the following equations [17]:

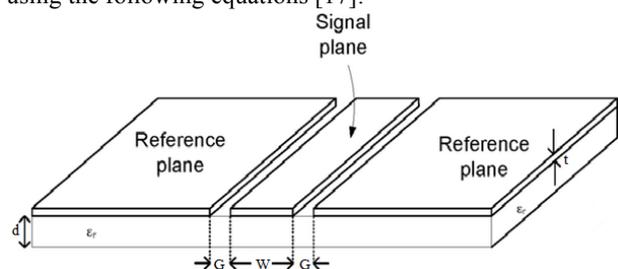


Fig. 1. Coplanar waveguide (CPW) line [17]

There are four geometric parameters: the Gap G, the conductor width W, metal thickness t and the substrate thickness d. The characteristic impedance and the effective permittivity are given approximately below:

Effective permittivity

$$\epsilon_{re} = \frac{\epsilon_r + 1}{2} \{A + B\} \quad (1)$$

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Where

$$\left[\frac{1}{\pi} \ln \left(2 \frac{1+\sqrt{k'}}{1-\sqrt{k'}} \right) \right]^{-1} \quad \text{if } 0.707 < k < 1 \quad (4)$$

$$A = \tanh \left[0.775 \ln \left(\frac{d}{G} \right) + 1.75 \right]$$

$$B = \left(\frac{kG}{d} \right) [(0.04 - 0.7k) + 0.01(1 - 0.1\epsilon_r)(0.25 + k)]$$

$$k = \frac{W}{W + 2G}$$

Characteristic Impedance

$$Z_0 = \frac{30\pi}{\sqrt{\epsilon_{re}}} \frac{K'(k)}{K(k)} \quad (2)$$

where $K(k)$ is a complete elliptical function of the first kind.

We have

$$k' = \sqrt{1 - k^2} ; K'(k) = K(k')$$

and

$$\frac{K'(k)}{K(k)} = \left[\frac{1}{\pi} \ln \left(2 \frac{1+\sqrt{k'}}{1-\sqrt{k'}} \right) \right] \quad \text{if } 0 < k < 0.707 \quad (3)$$

The CPW offers many advantages, which include the following:

- It can work to extremely high frequencies (100 GHz or more).
- Good circuit isolation can be achieved using a CPW. Many examples of high-isolation RF switches have used a grounded CPW to get 60 dB isolation or more.

After the validation of the design of this CPW line, we have introduced a modification into this CPW line permitting us to achieve a bandpass filter. The technique used, is based on the insertion of two lines coupled to the centered line and to enlarge the bandwidth we have used the periodic structure technique.

The bandpass filter is designed and simulated by using Momentum integrated into ADS solver. The optimization of such circuit is done by increasing the meshing density. After many series of optimization, we have validated the bandpass filter presented in Fig.2. The periodicity of the structure provides a wide frequency bandwidth behavior.

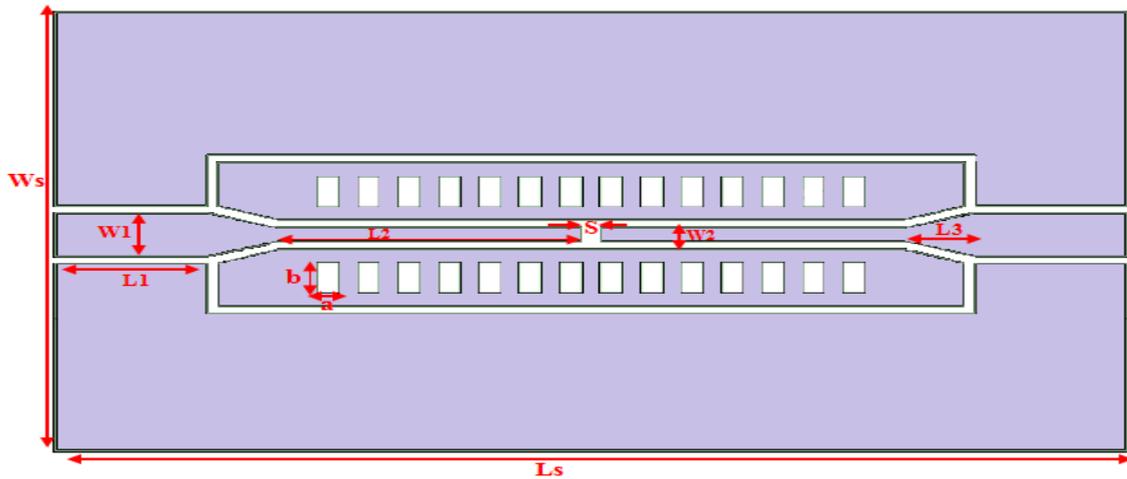


Fig.2. The proposed bandpass filter

The different optimized parameters are shown in Table 1

Table 1. values of the different parameters of the bandpass filter

Parameters	Values, mm
Ws	31
Ls	53
W1	3
L1	7.5
W2	1
L2	15
L3	3.5
s	1
a	1
b	2

This filter is mounted on an FR4 substrate having a thickness of 1.6mm, a dielectric permittivity $\epsilon_r = 4.4$ and

loss tangent $\tan\delta = 0.025$. Fig.3 indicates that the bandpass filter presents a wide frequency band from 1.283 to 3.337 GHz corresponding to -0.6dB of insertion loss and a reflection coefficient less than -10dB. As we shown in Fig.3, we have a good rejection far from the bandwidth.

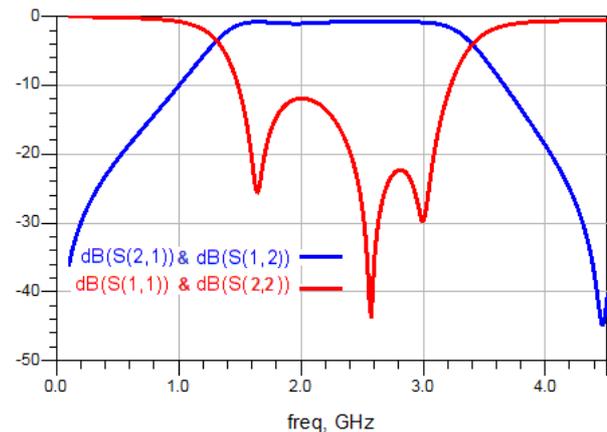


Fig. 3. S-parameters versus frequency of the designed filter

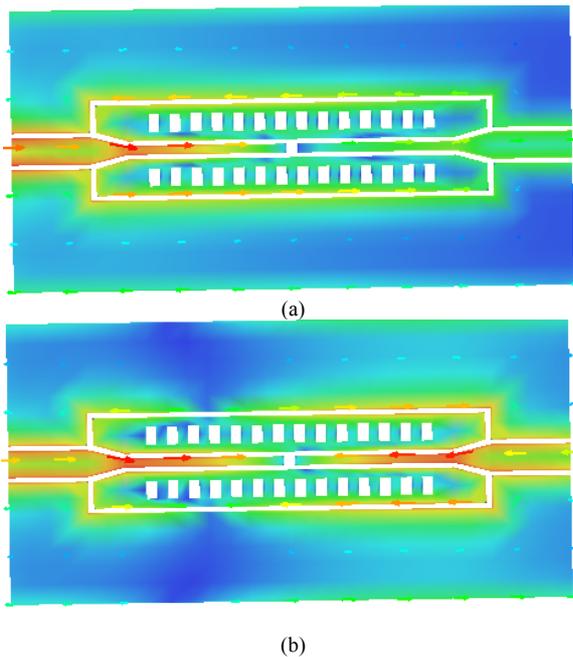


Fig. 4. Presents the current distribution (a) at 1GHz and (b) at 2.3 GHz.

Fig.4 presents the current distribution for a frequency 1GHz and 2.3GHz respectively out of and in the bandwidth. In order to compare the simulation results obtained by using ADS which is a 2D electromagnetic solver based on the moment method, also to take into account the dimensions of substrate, we have used another 3D electromagnetic solver HFSS.

The dimensions of the substrate are 35 X 31mm². As depicted in Fig.5, we have obtained nearly the same simulation results by using ADS and HFSS.

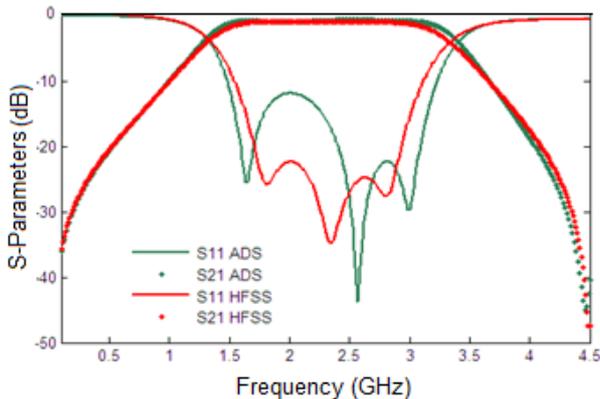


Fig. 5. Comparison results between HFSS and ADS of the proposed filter

3. Measurement results and discussion

After the validation of the proposed bandpass filter into simulation, we have conducted the fabrication of the final circuit as shown in Fig.6.

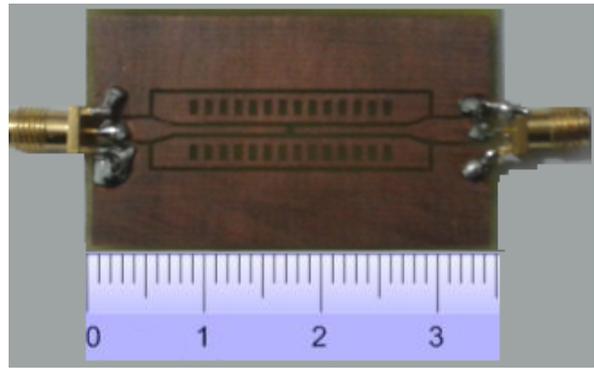


Fig. 6. Photograph of the fabricated Bandpass Filter

The achieved bandpass filter is measured by using a VNA from R&S, and 3.5mm Calibration Kit. The S parameters measured results are presented in Fig.7, which demonstrate a good agreement between simulation and measurement. As we can conclude, we have obtained a bandwidth of 2.054GHz with a good insertion loss. The final proposed bandpass filter can be used for DCS, ISM and WLAN applications.

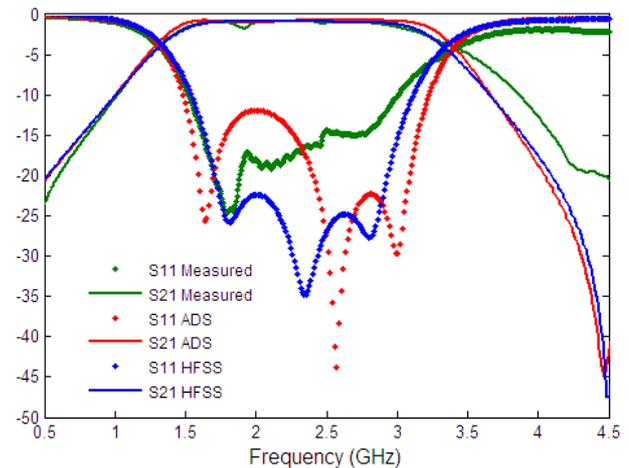


Fig. 7. Simulation and measurement results of the bandpass filter

4. Conclusion

This study has come with a novel CPW wide frequency bandpass filter which operates in the bandwidth from 1.283 to 3.337 GHz with a center frequency of 2.31GHz. This structure is compact, low cost and easy for integration with radiofrequency circuits. The final proposed bandpass filter presents good performances in term of insertion loss in a wide frequency band of 2.05GHz and a good rejection. These results are due to the integration of periodic structures based on optimized rectangular slots. The different steps followed to achieve such circuit can be followed to match this structure to other frequency bandwidth.

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