

Investigation On GFDM System For 5G Applications Over Fading Channels

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Abstract

The main goal of this paper is to investigate a generalized frequency division multiplexing (GFDM) system in Rician and Weibull fading settings utilizing the maximal ratio transmission (MRT) scheme. Now a day, most communication devices require low latency and low consumption of energy. In the literature, various multicarrier techniques are addressed and GFDM is one such technique that is new formulation research for future generations of mobile services. One of the major advantages of the GFDM technique is low out-of-band radiation. This paper initially explores the symbol error rate (SER) expression analysis in Rician and Weibull fading using the proposed GFDM-MRT system. Later on, performance is evaluated with MATLAB simulations for various simulation parameters such as the number of transmitting antennas, different roll-off factors, and various fading parameters. The performance is improved by 8dB to achieve the symbol error rate of 0.01 when we use the number of transmitting antennas ($N_t = 4$) compared to a single antenna ($N_t = 1$). Finally, it can be concluded that GFDM-MRT techniques are more reliable for high-speed communications.

Keywords: GFDM, Maximal Ratio Transmission, symbol error rate, Rician fading, Weibull Fading, 5G network.

1. Introduction

It is expected that the 5G cellular networks of fifth-generation will tackle several things at a time to meet user's satisfaction. To meet their expectations, 5G systems require very little latency for the tactile internet, a loose synchronization for the Internet of Things (IoT), reliability, efficient and robust high throughput to communicate via bit pipe communication, large coverage area, and a dynamic allocation of the spectrum with the low value of out of band emission. The main factor that distinguishes between GFDM and OFDM is that number of subcarriers are non-orthogonal to each other in GFDM [1]. One more major advantage with GFDM is that cyclic prefixes (CP) are not added to each subcarrier so a lot of bandwidth is saved. In GFDM, only one CP is added to the combination of subcarriers, hence, we receive the same bits at the receiver that are transmitted from the transmitter. For carrier aggregation, OFDM was having a high Out of Band (OOB) emission and it is low for GFDM [2]. GFDM system is less complex, achieves low OOB and it is promising 5G solution is stated in [3-4]. In [5], the authors discussed that GFDM is a flexible technology that overcomes the drawbacks presented in 4G technology. As a result, it suggests that GFDM is backward compatible with long-term evolution's accumulated knowledge.

The OOB emission of GFDM can be reduced if there is a smooth transition between the blocks of GFDM. The guard band is used in between the GFDM blocks by erasing the first sub-symbol and there will be the orientation of signal edges towards zero corresponding to that. This makes the transition between the blocks of GFDM smooth. This whole process is named guard-symbol GFDM (GS-GFDM) [6]. Generally, GFDM is a waveform that is non-orthogonal but

it can be made orthogonal by using various pulse shaping filters. It can also be done by making use of the combination of GFDM and orthogonal quadrature amplitude modulation (OQAM).

GFDM is a less complex approach, it can implement an LTE master clock for 5G Physical layers. Along with that the time-frequency structure of the nowadays cellular systems can also be implemented in [7]. Various circular pulse shaping filters are addressed in [8-10] which are used in the GFDM system to meet the requirements in the latest technologies. The GFDM signal is generated by multiplying and concatenating input symbols with an appropriate prototype filter [11].

ISI can be removed but noise value is enhanced using a zero forced (ZF) receiver. Further, the efficiency of the GFDM receiver can be increased with a minimum mean square estimation (MMSE) receiver [12]. ICI reduction approaches are suggested in [13]. A pre-coded GFDM system is discussed in [14]. To minimize ICI and the complexity of the receiver, the scheme was suggested in [14]. In [11], GFDM, OFDM, and single carrier frequency division (SC-FDM) analysis and their PAPRs performances were compared and it stated that GFDM achieves lower PAPR. The symbol error rate (SER) expression over the AWGN channel for the GFDM system with a ZF receiver is shown in [5].

The multiple-input and multiple-output (MIMO) based GFDM analysis is described in [15-16] which receiver complexity is more. This method uses a maximal ratio combining (MRC) scheme before demodulation. A large-scale MIMO transmission GFDM scheme is described in [17]. In [18], V-BLAST and spatial modulation schemes are used in the GFDM system and bit error rate (BER) performance is evaluated. The complexity of identification of MIMO-GFDM signals analysis is given in [19]. The detection complexity is further reduced in the MIMO-

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GFDM system using the Montecarlo algorithm in [20-21]. MIMO structure and MRT also reduces the complexity in [22-23]. Weibull fading is a basic statistical model that can be used in both indoor and outdoor settings, according to studies [31]. The importance of the Weibull fading channel in digital modulation systems is convincingly demonstrated in [32]. Some detailed analysis about the Weibull fading channel is provided in [33].

With the use of Maximal ratio transmission (MRT), receiver complexity in MIMO systems is reduced. There is not much work is addressed in the literature related to GFDM with MRT. The MRT-based GFDM system performance is evaluated over Nakagami- m fading channel in [24]. The above-stated references are useful to analyze the performance of GFDM with the MRT scheme in the Rician fading channel.

The remaining paper is structured in other four sections. The proposed GFDM based MRT scheme is described in section-2. Section-3 deals with the SER analysis in Rician and Weibull fading. Simulation analysis followed by conclusions is given in section-4 and section-5 respectively.

2. System Model Description

The proposed GFDM based MRT system model is shown in Fig. 1. The proposed system is having a transmitter and receiver. The transmitter consists of an encoder, mapper, and other various blocks. The vectorial data (\mathbf{b}) in the form of bits given as input to the encoder. The encoder converts the input from low bit-rate data stream into high bit-rate data stream and the output of the data vector is (\mathbf{b}_c). The output of the encoder is given as input to the mapper and it produces output as $N \times 1$ data vector (\mathbf{d}). This vectorial data is given as input to the GFDM modulator which consists of N elements. The vectorial data (\mathbf{d}) is decomposes into K groups M symbols as follows.

$$\mathbf{d} = [(d_0)^T, (d_1)^T, \dots, (d_{K-1})^T]^T \quad (1)$$

with

$$d_k = [d_{k,0}, d_{k,1}, \dots, d_{k,M-1}]^T \quad (2)$$

In eq. (2), $d_{k,m}$ is data symbol which is transmitted through k -th subcarrier at m -th time slot and $g_{k,m}(\mathbf{n})$ is filter coefficient. Let us assume that the GFDM block occupies K subcarriers, each subcarrier consists of M data symbols and it produces $N = KM$ samples. With GFDM modulator, samples are filtered with a corresponding transmit filter is given as [11]

$$g_{k,m}[n] = g[(n - mk) \bmod N] e^{-\frac{j2\pi kn}{K}} \quad (3)$$

The exponential term conducts frequency domain shift, and $g_{k,m}(\mathbf{n})$ is a time and frequency shifted version of $g(\mathbf{n})$. Finally, all the transmitted symbols are superimposed at one place that leads to GFDM signal which is given as $\mathbf{x}(\mathbf{n})$ in [11]

$$\mathbf{x}[n] = \sum_{k=0}^{K-1} \sum_{m=0}^{M-1} d_{k,m} g_{k,m}[n], \quad n = 0, 1, \dots, KM - 1 \quad (4)$$

The pulse-shaping filter samples can be shown as follows

$$g_{k,m} = [g_{k,m}[0], g_{k,m}[1] \dots g_{k,m}[MK - 1]]^T \quad (5)$$

and matrix representation of eq. (4) is [12]

$$\mathbf{x} = A\mathbf{d} \quad (6)$$

where A is a $KM \times KM$ dimension matrix which is also known as GFDM modulation matrix and is represented as [5]

$$A = [g_{0,0} \dots g_{K-1,0} g_{0,1} \dots g_{K-1,M-1}] \quad (7)$$

A cyclic prefix (CP) and cyclic suffix (CS) are added after GFDM block and then signal components are weighted with MRT coefficients as;

$$x_i = w_i x \quad (8)$$

where w_i is weighting factor (MRT coefficient) for i -th antenna and ($i = 1, 2, \dots, N_t$) [22];

$$w_i = \frac{h_i^*}{h_F} \quad (9)$$

$$h_F = \|h\| = \sqrt{\sum_{i=1}^{N_t} |h_i|^2}$$

In eq. (9), h_i is channel coefficient. h_F Frobenius norm of channel vector $h = [h_1, h_2, \dots, h_{N_t}]$.

Finally, the GFDM signal is multiplied with MRT coefficients is received at the receiver and its mathematical representation is

$$\mathbf{r} = \sqrt{P_t} \sum_{i=0}^{N_t} h_i w_i \mathbf{x} + \mathbf{w} = \sqrt{P_t} h_F \mathbf{x} + \mathbf{w} \quad (10)$$

Where \mathbf{w} is a noise vector $w \sim (0, \sigma_w^2)$. Later on, power is normalized by $P_t = 1/N_t$ at each antenna, so that channel coefficient in eq. (9) is equalized. Finally, an output signal from the equalizer is demodulated by matched filter (MF), ZF, and MMSE. The expression for the demodulated signal is [5]

$$\hat{\mathbf{d}} = B\mathbf{y} \quad (11)$$

where B is a demodulation matrix.

The demodulation matrix for the MF receiver is $B_{MF} = A^H$ which maximizes SNR and self-interference. Likely, for MMSE receiver B matrix is

$$B_{MMSE} = (R_n^2 + A^H H^H A H)^{-1} A^H H^H$$

which balances self-interference and noise enhancement and R_n^2 is the noise covariance matrix. Similarly, the B matrix for the ZF receiver is $B_{MF} = A^{-1}$. While the ZF receiver eliminates self-interference, it significantly improves noise efficiency.

The noise enhancement factor (NEF) ' ξ ' represents the amount of reduction in SNR value when uses ZF receiver and its mathematical expression is [5]

$$\xi = \sum_{i=0}^{MK-1} |[B_{ZF}]_{k,i}|^2 \quad (12)$$

where ‘ ξ ’ is equal for all $k = 0, 1, \dots, MK - 1$.

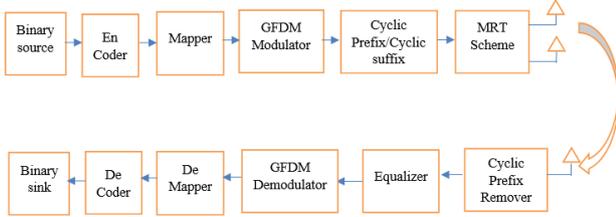


Fig. 1. Proposed GFDM Transceiver with MRT Scheme.

3. Symbol Error Rate Analysis

This section gives the analysis of GFDM based MRT scheme SER performance with ZF receiver in Rician and weibull fading environment. The usage of the ZF receiver in the proposed system reduces the self-interference but increases the noise value. The SER performance is evaluated using the QAM modulation scheme in the Rician and weibull channel. The channel impulse response of length N_{ch} can be represented as

$$h = [h_0, \dots, h_{N_{ch}-1}]^T \quad (13)$$

The received signal mathematical representation at the receiver is

$$r = Hx + w \quad (14)$$

In the above expression r and x are received and transmitted information respectively. Where $H = circ\{\bar{h}\}$ and \bar{h} is a zero-padded version of h of the same length. For AWGN environment $H=I$, where I is identity matrix. For the different fading environments in the wireless channel, H value varies. In this paper, we are considering Rician and weibull fading in the wireless channel since it can be modeled as most of the cases because it consists of a line of sight (LOS) component.

3.1. Rician Channel Model

The Rician channel can be modeled if the signal amplitude in the wireless channel follows the Rician distribution. The envelopes of channel coefficients are $|h_i|$ for $i = 1, 2, \dots, N_t$ and PDF is given as [27].

$$f_{|h_i|}(|h_i|) = \left(\frac{1+K}{\bar{h}_i}\right) \exp\left[-\frac{(1+K)h_i + K\bar{h}_i}{\bar{h}_i}\right] I_0\left[\sqrt{\frac{4K(1+K)h_i}{\bar{h}_i}}\right]; \quad 0 \leq K < \infty \quad (15)$$

Where K is the Rician fading parameter

The instantaneous SNR value is

$$\gamma = \frac{P_t E_s}{\xi N_0} h_F^2 \quad (16)$$

In eq. (16), E_s and N_0 are average energy per symbol and noise power spectral density respectively. From eq. (9), the envelope of h_F can be computed as

$$h_F = \sqrt{X_1^2 + X_2^2 + \dots + X_{2mN_t}^2} \quad (17)$$

where $X_i \sim (0, \sigma_x^2)$ and $(i = 1, 2, \dots, 2mN_t)$ and $\bar{K} = KN_t$ [25], then the expression for PDF is

$$p_{h_F}(h_F) = \left(\frac{1+\bar{K}}{\bar{h}_F}\right) \exp\left[-\frac{(1+\bar{K})h_F + \bar{K}\bar{h}_F}{\bar{h}_F}\right] I_0\left[\sqrt{\frac{4\bar{K}(1+\bar{K})h_F}{\bar{h}_F}}\right]; \quad 0 \leq K < \infty \quad (18)$$

Then, the PDF in terms of SNRs is given in [26];

$$p_\gamma(\gamma) = \left(\frac{1+\bar{K}}{\bar{\gamma}}\right) \exp\left[-\frac{(1+\bar{K})\gamma + \bar{K}\bar{\gamma}}{\bar{\gamma}}\right] I_0\left[\sqrt{\frac{4\bar{K}(1+\bar{K})\gamma}{\bar{\gamma}}}\right]; \quad 0 \leq K < \infty \quad (19)$$

where $\bar{\gamma}$ is the average SNR value or $\bar{\gamma} = E[\gamma]$.

3.2. SER of GFDM-MRT

This section gives the exact expressions of SER of the GFDM-MRT system over the non-fading environment, Rician and weibull fading environment.

3.3 Non-fading (AWGN) Environment

The SNR is equally adjusted by NEF for GFDM at the receiver side. Hence, both OFDM SER and GFDM SER expressions for the AWGN environment are almost the same and they are differed in equivalent SNR [28]. The expression for SER under AWGN using GFDM system is [5];

$$P_{SER,AWGN}(\gamma) = 2\left(\frac{p-1}{p}\right) \text{erfc}(\sqrt{\gamma}) - \left(\frac{p-1}{p}\right)^2 \text{erfc}^2(\sqrt{\gamma}) \quad (20)$$

Where

$$\gamma = \frac{3RT}{2(2^\mu-1)} \frac{E_s}{\xi N_0} \text{ and } r = \frac{NM}{NM+N_{CP}+N_{CS}} \quad (21)$$

In eq. (20) and (21), $p = \sqrt{2\mu}$, μ represents the number of bits, N_{CP} , N_{CS} are the length of CP and CS respectively. N and M are number of subcarriers and sub-symbols.

The SER expression for different fading environments can be evaluated by averaging the error rates AWGN over PDF of other fading channels. It can be calculated using [5]

$$P_{SER} = \int_0^\infty P_{AWGN}(\gamma) P_\gamma(\gamma) d\gamma \quad (22)$$

In eq. (22), $P_\gamma(\gamma)$ represents the PDF of different fading channels.

3.4 Rician Fading Environment

To calculate SER expression in Rician fading, we require a PDF of Rician fading. The PDF expression is shown in eq. (19), it can be further modified by expressing it in infinite series form of a zeroth model of Bessel function [29];

$$I_0(x) = \sum_{q=0}^\infty \frac{\left(\frac{x^2}{4}\right)^q}{(q!)^2} \quad (23)$$

The modified PDF expression for the Rician fading environment is given in [25]

$$P_\gamma(\gamma) = \frac{1+K}{\bar{\gamma}_r} e^{-K} \sum_{q=0}^{\infty} \frac{1}{(q!)^2} \left(\frac{K(1+K)}{\bar{\gamma}_r}\right)^q \gamma^q \exp\left(-\frac{\gamma(1+K)}{\bar{\gamma}_r}\right) \quad 0 \leq K < \infty \quad (24)$$

Now, SER expression for Rician fading can be computed by substituting eq. (20) and eq. (24) in eq. (22), the bounded SER expression for GFDM system with single antenna is [25];

$$P_{SER,Ric}(\gamma) = \frac{2(p-1)}{p} I_3(\bar{\gamma}_r) - \left(\frac{p-1}{p}\right)^2 I_4(\bar{\gamma}_r) \quad (25)$$

Where $I_3(\bar{\gamma}_r)$ and $I_4(\bar{\gamma}_r)$ are expressed as given below;

$$I_3(\bar{\gamma}_r) = \frac{1+K}{\bar{\gamma}_r} e^{-K} \sum_{q=0}^{\infty} \frac{1}{(q!)^2} \left(\frac{K(1+K)}{\bar{\gamma}_r}\right)^q \frac{\Gamma(q+\frac{3}{2})}{\sqrt{\pi}(q+1)} {}_2F_1\left[q + 1, q + \frac{3}{2}; q + 2; + \left(\frac{1+K}{\bar{\gamma}_r}\right)\right] \quad (26)$$

$$I_4(\bar{\gamma}_r) = e^{-K} \sum_{q=0}^{\infty} \frac{K^q}{(q!)^2} \left(1 - \frac{4}{\pi} \sum_{j=0}^q \frac{\left(\frac{1+K}{\bar{\gamma}_r}\right)^j}{2j+1} {}_2F_1\left[j + \frac{1}{2}, j + 1; j + \frac{3}{2}; -\left(\frac{1+K}{\bar{\gamma}_r} + 1\right)\right]\right) \quad (27)$$

Similarly, for multiple antennas (N_t) case, SER expression for GFDM based MRT system is obtained by changing K to KN_t , the bounded SER expression for GFDM based MRT system with multiple antennas is

$$P_{SER,Ric}(\gamma) = \frac{2(p-1)}{p} I_3(\bar{\gamma}_r) - \left(\frac{p-1}{p}\right)^2 I_4(\bar{\gamma}_r) \quad (28)$$

$$I_3(\bar{\gamma}_r) = \frac{1+KN_t}{\bar{\gamma}_r} e^{-K} \sum_{q=0}^{\infty} \frac{1}{(q!)^2} \left(\frac{KN_t(1+KN_t)}{\bar{\gamma}_r}\right)^q \frac{\Gamma(q+\frac{3}{2})}{\sqrt{\pi}(q+1)} {}_2F_1\left[q + 1, q + \frac{3}{2}; q + 2; + \left(\frac{1+KN_t}{\bar{\gamma}_r}\right)\right] \quad (29)$$

$$I_4(\bar{\gamma}_r) = e^{-KN_t} \sum_{q=0}^{\infty} \frac{(KN_t)^q}{(q!)^2} \left(1 - \frac{4}{\pi} \sum_{j=0}^q \frac{\left(\frac{1+KN_t}{\bar{\gamma}_r}\right)^j}{2j+1} {}_2F_1\left[j + \frac{1}{2}, j + 1; j + \frac{3}{2}; -\left(\frac{1+KN_t}{\bar{\gamma}_r} + 1\right)\right]\right) \quad (30)$$

where

$$\bar{\gamma}_r = \frac{3R_T \sigma_r^2 E_s}{(2^\mu - 1) \xi N_0} \quad (31)$$

In the above eq. (31), $\bar{\gamma}_r$ is equivalent SNR in a Rician fading environment. Where ${}_2F_1[., .; .;]$ denotes the Gauss hypergeometric function [30]. It is assumed that σ_r^2 value is 0.5. If we substitute $K = 0$ for both single and multiple antennas cases, the expressions give the SER expressions for the Rayleigh fading environment. For $K = 0$, our simulation (Fig.2, black line) is exactly matching with the simulation (Fig.6, curve (i)) given in [25]. For $N_t = 1$, eq. (25) and eq. (28) are exactly match with each other.

4 Nakagami- m Fading Environment

The PDF expression for Nakagami- m fading environment is given in [24] as

$$p_\gamma(\gamma) = \left(\frac{m}{\bar{\gamma}}\right)^m \frac{\gamma^{m-1}}{\Gamma(m)} e^{-\frac{m\gamma}{\bar{\gamma}}} \quad (32)$$

To calculate SER expression in Nakagami- m fading, we require a PDF of Nakagami- m fading which is shown in eq. (32). Now, SER expression for Nakagami- m fading can be calculated by substituting equ. (20) and equ. (32) in equ. (22), the bounded SER expression for GFDM system with single antenna is given in [24];

$$P_{SER,Nak} = 2C_1 C_2^m \frac{\Gamma(m+\frac{1}{2})}{\sqrt{\pi}\Gamma(m+1)} {}_2F_1\left[m, m + \frac{1}{2}; m + 1; -C_2\right] - C_1^2 \left[1 - \frac{4}{\pi} \sum_{j=0}^{m-1} \frac{C_2^j}{2j+1} {}_2F_1\left[j + \frac{1}{2}, j + 1; j + \frac{3}{2}; -(C_2 + 1)\right]\right] \quad (33)$$

where C_1 and C_2 are expressed as follows;

$$C_1 = \frac{\sqrt{2^\mu - 1}}{\sqrt{2^\mu}}, \quad C_2 = \frac{m}{\bar{\gamma}_n} \quad (34)$$

Similarly, for multiple antennas (N_t) case, SER expression for GFDM based MRT system is obtained by changing m to mN_t , the bounded SER expression for GFDM based MRT system with multiple antennas is given in [24];

$$P_{SER,Nak} = 2C_1 C_2^{mN_t} C_4 {}_2F_1\left[mN_t, mN_t + \frac{1}{2}; mN_t + 1; -C_3\right] - C_1^2 \left[1 - \frac{4}{\pi} \sum_{j=0}^{mN_t-1} \frac{C_3^j}{2j+1} {}_2F_1\left[j + \frac{1}{2}, j + 1; j + \frac{3}{2}; -(C_3 + 1)\right]\right] \quad (35)$$

where C_3 and C_4 are expressed as follows

$$C_3 = \frac{mN_t}{\bar{\gamma}_n}, \quad C_4 = \frac{\Gamma(mN_t+\frac{1}{2})}{\sqrt{\pi}\Gamma(mN_t+1)} \quad (36)$$

$$\bar{\gamma}_n = \frac{3R_T P_t N_t \sigma_n^2 E_s}{(2^\mu - 1) \xi N_0} \quad (37)$$

In the above eq. (33), $\bar{\gamma}_n$ is equivalent to SNR in the Nakagami-fading environment. It is assumed that σ_n^2 value is 0.5. If we substitute $m = 1$ for both single and multiple antennas cases, the expressions give the SER expressions for the Rayleigh fading environment. For $m=1$, our simulation (Fig.2) is exactly matching with the simulation (Fig.2) given in [24]. For $N_t = 1$, eq. (33) and eq. (35) are exactly match with each other. For $m = 1$ and $K = 0$, eq. (25) and eq. (33) gives the same results and those two equations merge to Rayleigh's fading environment.

5 Weibull Fading Environment

The modified PDF expression for the Rician fading environment is given in [34];

$$P_\gamma(\gamma) = \left(\frac{v}{2(a\bar{\gamma})^{\frac{v}{2}}}\right) \gamma^{\frac{v}{2}-1} \exp\left(-\left(\frac{\gamma}{a\bar{\gamma}}\right)^{\frac{v}{2}}\right) \quad (38)$$

Now, SER expression for Weibull fading can be computed by substituting equ. (20) and equ. (38) in equ. (22), the bounded SER expression for GFDM system with single antenna is [33];

where $a = 1/\Gamma(1 + 2/v)$.

$$P_{wbl}(e) = \frac{2(p-1)}{p} \frac{\frac{v}{2}}{(a\bar{\gamma})^{\frac{v}{2}}} I_3(\bar{\gamma}_{wb}) - \left(\frac{p-1}{p}\right)^2 \frac{\frac{v}{2}}{(a\bar{\gamma})^{\frac{v}{2}}} I_4(\bar{\gamma}_{wb}) \quad (39)$$

Where

$I_3(\bar{\gamma}_{wb})$ and $I_4(\bar{\gamma}_{wb})$ are expressed as given below;

$$I_3(\bar{\gamma}_{wb}) = \int_0^\infty \gamma^{\frac{v}{2}-1} e^{-\frac{\gamma}{(a\bar{\gamma}_{wb})^{\frac{v}{2}}}} \operatorname{erfc}(\sqrt{\gamma}) d\gamma \quad (40)$$

$$I_4(\bar{\gamma}_{wb}) = \int_0^\infty \gamma^{\frac{v}{2}-1} e^{-\frac{\gamma}{(a\bar{\gamma}_{wb})^{\frac{v}{2}}}} \operatorname{erfc}^2(\sqrt{\gamma}) d\gamma \quad (41)$$

Where

$$\bar{\gamma}_{wb} = \frac{3R_T \sigma_{wb}^2 E_s}{(2^\mu - 1) \xi N_0} \quad (42)$$

From [33], $I_3(\bar{\gamma}_{wb})$ and $I_4(\bar{\gamma}_{wb})$

$$I_3(\bar{\gamma}_{wb}) = \frac{2(a\bar{\gamma}_{wb})^{\frac{v}{2}}}{v} - \frac{\left(\frac{k}{2}\right)^{\frac{1}{2}} (\lambda)^{\frac{v}{2}}}{\sqrt{\pi}(2\pi)^{\frac{\lambda+k-2}{2}}} G_{2\lambda, k+\lambda}^{k+\lambda, \lambda} \left[\frac{\lambda^{\lambda-k}}{(a\bar{\gamma}_{wb})^{\frac{vk}{2}}} \middle| \begin{array}{l} \Delta\left(\lambda, \frac{1-v}{2}\right), \Delta\left(\lambda, 1 - \frac{v}{2}\right) \\ \Delta(k, 0), \Delta\left(\lambda, -\frac{v}{2}\right) \end{array} \right] \quad (43)$$

$$I_4(\bar{\gamma}_{wb}) = \frac{2(a\bar{\gamma}_{wb})^{\frac{v}{2}}}{v} \left[1 - \frac{2 \sum_{i=0}^{\infty} \frac{(-1)^i}{i!} \left(\frac{k}{2}\right)^{\frac{1}{2}} (\lambda)^{\frac{i-1}{2}}}{\sqrt{\pi}(2\pi)^{\frac{\lambda+k-2}{2}}} G_{2\lambda, k+\lambda}^{k+\lambda, \lambda} \left[\frac{\lambda^{\lambda-k}}{(a\bar{\gamma}_{wb})^{\frac{vk}{2}}} \middle| \begin{array}{l} \Delta\left(\lambda, \frac{1}{2} - i\right), \Delta(\lambda, -i) \\ \Delta(k, 0), \Delta\left(\lambda, -i - \frac{1}{2}\right) \end{array} \right] \right] \quad (44)$$

Similarly, for multiple antennas (N_t) case, SER expression for GFDM based MRT system is obtained by changing K to KN_t .

4. Simulation Analysis

This section discusses the simulation results and their analysis. All the simulations are performed with simulation values such as number of subcarriers $K=64$, length of CP $N_{CP}=8$ and length of $N_{CS}=0$.

4.1 Specifications used for simulation

Parameter	Variable	Value
Modulation Scheme	μ (Modulation Index)	QPSK , 16-QAM
Sub-carriers	K	64
Block-length	M	16
Filter type	-	RRC
Roll-off factor	α	0.1,0.6,0.9
Channel	$h(n)$	1, for AWGN
Cyclic prefix	CP	-
Fading Channels	-	Rician, Weibull
Fading Parameter	K	0,1,2,3 If $K=0$ Channel is Rayleigh fading $K=\infty$ Channel is AWGN
Transmitting Antennas	N_t	4

Fig. 2 represents the SER analysis of GFDM-MRT based system for various values of SNRs using multiple antennas at the transmitter ($N_t = 1,2,3,4$) and with a roll-off factor $\alpha = 0.1$. From the simulation, it is observed that simulation is evaluated for Rayleigh fading ($K = 0$) environment which is a special case of Rician fading with Rician fading parameter $K=0$. It is also observed that SER performance decreases as the number of antennas increases. In [24] SER performance was calculated for only $N_t=1$, the value of SER is 0.13×10^{-2} but in this paper we calculate SER performance for $N_t = 1, 2, 3, 4$ respectively. At $N_t = 4$ SER performance is compared with $N_t=1$ in [24] minimized the SER to 99.97%. Finally, it can be concluded that the GFDM-MRT scheme with $N_t = 4$ gives 10dB, 4dB, and 2dB SNR gain for $N_t = 1, 2, 3$ transmit antennas at $\text{SER}=10^{-2}$. Fig. 2 also compares the simulation results of [24] for different values of N_t , $K = 0$, and $\alpha = 0.1$.

Fig. 3 represents the SER analysis of GFDM-MRT based system for various values of SNRs using multiple antennas at the transmitter ($N_t = 2$), various Rician fading parameters $K = (0,1,2,3)$ and with a roll-off factor $\alpha = 0.1$. The curve for $K = 0$ is exactly matches with Rayleigh fading conditions and gives the same SER performance which matches with previous work [24]. But here, we can infer that as an increase in Rician fading parameter (K) from 0 to 3, the SER decreases.

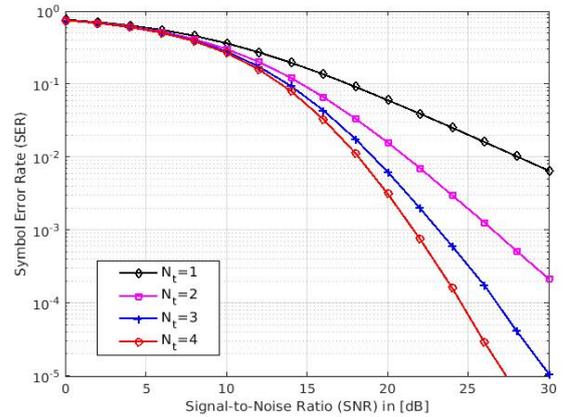


Fig. 2. SER vs SNR performance with the various number of transmitting antennas.

For a particular case at $\text{SNR}=15\text{dB}$, the error values for $K=0, 1, 2, 3$ are respectively 0.01596, 0.0103, 0.0060 and 0.003. At $K=4$ SER performance is compared with $K=0$ [24] i.e. approximately there is an 81.2% decrease in error from $K=0$ to $K=3$. Finally, it can be concluded that GFDM-MRT scheme with $N_t = 4$ gives 10dB, 4dB, and 2dB SNR gain for $N_t = 1, 2, 3$ transmit antennas at $\text{SER}=10^{-2}$.

Fig. 4 is drawn between SER and SNR for different roll-off factors ($\alpha = 0.1, 0.6, 0.9$), $N_t = 2$, $K = 2$ and using a 16-QAM modulation scheme. Fig. 4 also explains the effect of the NEF parameter ζ which plays a key role in GFDM. As the value of the roll-off factor increases from 0.1 to 0.9, there is a significant change in the SER curve because as ζ increases there is a wider overlap of the subcarriers which increases the NEF factor. The SER values are 0.0216, 0.0116, 0.0060 at $\text{SNR}=20\text{dB}$ for various values of $\alpha = 0.9, 0.6$ and 0.1 respectively. Here as α value decreases from 0.9

to 0.1, the SER value decreases by 72% but in literature[24] SER decreased by 50% as α value decreases from 0.9 to 0.1

Fig. 5 is drawn between SER and roll-off factor for different SNR values (10dB, 15dB, 20dB), $N_t = 3, K = 3$ and using 16-QAM modulation scheme. From the simulation it is observed that as SNR value increases from 10dB to 20dB, SER value decreases from 0.277 to 0.001 at $\alpha = 0.4$, it shows that there is an almost 95% improvement in SER with the increase in SNR. At a lower α value, the SER value is lower and it increases at higher α values. Finally, it can be concluded that to achieve less symbol error rate lower value at $\alpha=0.1$ and higher SNR=20dB values are always recommendable.

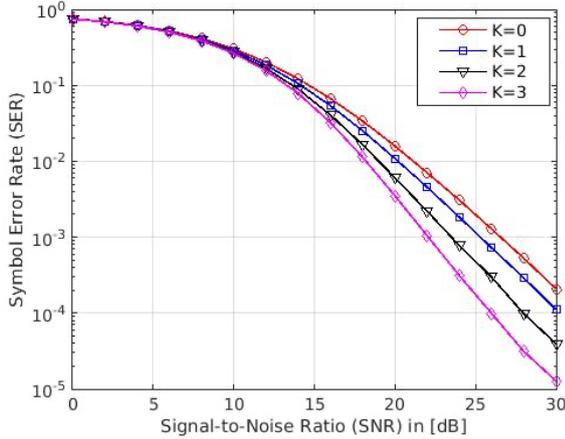


Fig. 3. SER vs SNR performance for various Rician fading parameters.

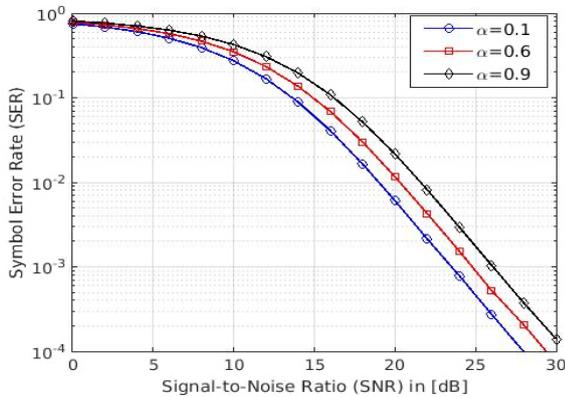


Fig.4. SER vs SNR performance for various Roll-off factors.

Fig. 6 is drawn between SER and SNRs for different modulation schemes (QPSK and 16-QAM), $K = 3, N_t = 3$ and $\alpha = 0.1$. From this simulation, we can state that the QPSK scheme achieves a lower value of SER compare to the 16-QAM modulation scheme. For a particular case, at SNR=10dB, SER values are 0.0251 and 0.0072 for 16-QAM and QPSK schemes.

Fig. 7 represents the SER performance of GFDM-MRT based system for various values of SNRs using multiple antennas at the transmitter ($N_t = 1,2,3,4$) and with a roll-off factor $\alpha = 0.1$ under the Weibull fading channel. In literature [33] only at $N_t = 1$ transmitter SER performance analysed. It is observed from Fig.7 that SER performance falls as N_t increases. For a particular case at SNR= 15dB, SER values are 0.04409, 0.03329, 0.02054 and 0.01554 for $N_t = 1, 2, 3, 4$ respectively. Finally, it can be concluded that the GFDM-MRT scheme with $N_t = 4$ gives 4dB, 3dB, and 2dB

SNR gain according to $N_t = 1, 2, 3$ transmit antennas respectively at SER= 10^{-2} .

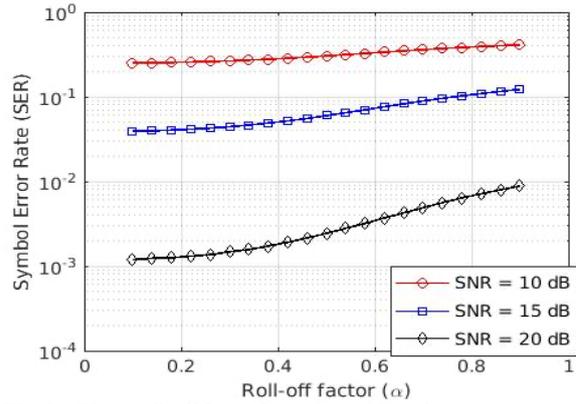


Fig. 5. SER vs roll-off factor for various SNR values.

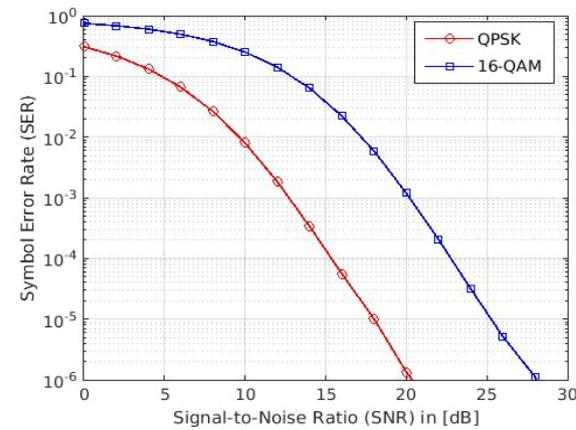


Fig.6. SER vs SNR performance for various modulation schemes.

Fig. 8 is drawn between SER and SNR for different roll-off factors ($\alpha = 0.1, 0.6, 0.9$), $N_t = 2$ and using a 16-QAM modulation scheme. Fig. 8 also explains the effect of the NEF parameter ζ which plays an important role in GFDM. The SER values are 0.04064, 0.02054, 0.01129 at SNR=16dB for various values of $\alpha = 0.9, 0.6$ and 0.1 respectively. As α value decreases from 0.9 to 0.1, the SER value decreases by 72.2%.

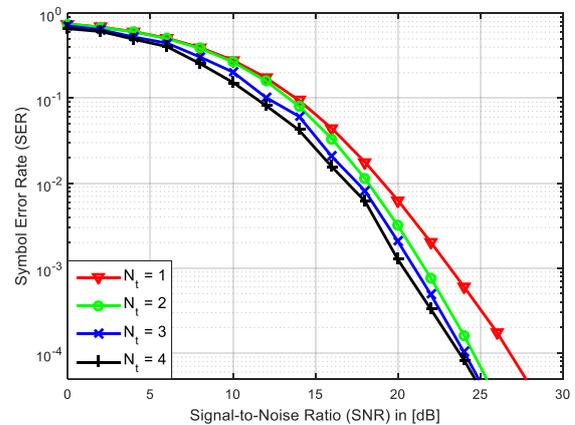


Fig.7. SER vs SNR performance with the various number of transmitting antennas.

Fig. 9 is drawn between SER and roll-off factor for different SNR values (10dB, 15dB, 20dB), $N_t = 3$ and using a 16-QAM modulation scheme. From the simulation, it is

observed that as SNR value increases from 10dB to 20dB, SER value decreases from 0.03525 to 0.05544 at $\alpha = 0.4$, which shows that there is an almost 57.2% improvement in SER with the increase in SNR. The SER value is less at lower values of α and it increases and is high at higher values of α .

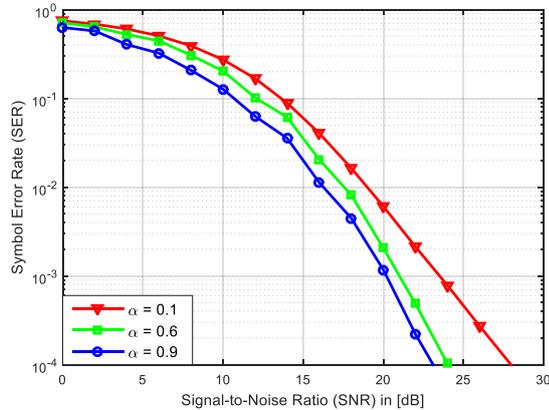


Fig.8. SER vs SNR performance for various Roll-off factors.

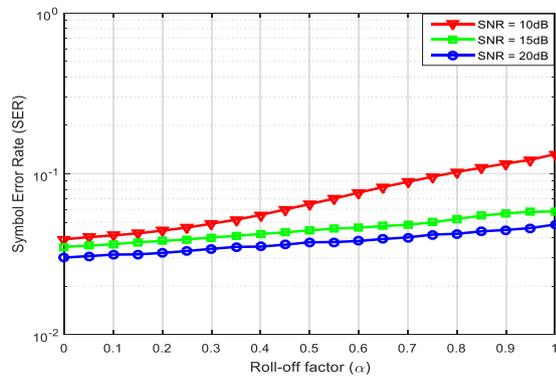


Fig.9. SER vs roll-off factor for various SNR values.

5. Conclusion

Under the Rician fading environment, the proposed GFDM-MRT scheme is suggested and its symbol error rate (SER) performance is investigated. Initially, the closed form of SER expression under Rician and Weibullfading environment for single and multiple antennas has provided. Later on, SER performance is evaluated with MATLAB simulations for various simulation parameters such as several transmitting antennas, different roll-off factors, and various fading parameters. We have also validated our simulations with the existing literature papers. The SNR performance is improved by approximately 6dB to achieve the symbol error rate of 0.01, when we use the number of transmitting antennas ($N_t = 4$) compared to a single antenna. ($N_t = 1$). Finally, it can be concluded that the GFDM-MRT technique is more reliable for high-speed communications.

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