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**Research Article** 

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### Performance of Electrocoagulation Processes for the Removal of COD and Ammonia from High Salinity Landfill-leachate using Iron or Aluminum Electrodes

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#### Abstract

Landfill leachate is characterized by a large fraction of low biodegradability organics. The present work aimed to evaluate and optimize the electrocoagulation (EC) process to remove chemical oxygen demand (COD) and NH<sub>4</sub>-N from highsalinity landfill leachate. The study was conducted using iron or aluminum electrodes while different parameters such as reaction time, current density, and pH were evaluated on the process's efficiency. The experimental results showed that by applying a current density of 12 mAcm<sup>-2</sup>, the COD removal after 240 minute electro-processing time was 78.5 % and 72.5% for iron and aluminum electrodes respectively. Also, the removal of NH<sub>4</sub>-N after 240 minutes at a current density of 12 mA cm<sup>2</sup> was 62 % and 54% for iron and aluminum electrodes respectively. This study demonstrates the feasibility of electrocoagulation to treat high-salinity landfill leachate without the need for a supporting electrolyte.

Keywords: landfill leachate; electrocoagulation; aluminum and iron electrodes

#### 1. Introduction

Sanitary landfills consist of one of the most applied solutions for municipal and industrial solid waste disposal. Undeniably, landfills contribute to gaseous (carbon dioxide, methane, and nitrous oxides) and liquid emissions (leachate), the latter being rich in organic and inorganic compounds, heavy metals, and other anthropogenic chemicals that can severely contaminate soils and freshwater bodies [1].

There is no typical composition for landfill leachate samples, and this is closely related to the landfill-age, the weather conditions prevailing on-site, the type and composition of solid wastes disposed therein, the moisture content of the waste body, and the availability of oxygen [2]. The biodegradability of landfill-leachate is affected by the landfill-age, and it is evaluated according to the BOD/COD ratio. Old landfill leachates (> 10-15 years) are characterized by BOD/COD ratio between 0.05 and 0.20, while for young landfills (< 5 years) this value is often higher than 0.50[3].

Landfill-leachate requires appropriate treatment before disposal to the environment. Several technologies have been applied for landfill-leachate treatment, including physical, chemical, and biological processes [4]. In some cases, landfill-leachate is co-treated with sewage at municipal wastewater treatment plants [5]. During the last years, electrochemical technologies were proposed as an alternative treatment approaches. Electrocoagulation is an advanced treatment process that combines electrochemical methods with conventional chemical coagulation to remove organic and inorganic compounds from landfill leachates [6-10]. During the electrocoagulation process, metallic ions are released into the wastewater by the applied electrical current and subsequently hydrolyzed to generate the desired coagulating species. Therefore, the coagulants are not

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supplemented externally into the solution, rather than generated in-situ following electro-dissolution of the aluminum or iron anodes [11].

During the electrocoagulation process with iron and aluminum electrodes, the following reactions occur:

A) Iron	electrodes:		
$Fe \rightarrow$	Fe <sup>2+</sup> +2e	(anode)	(1)

$Fe \rightarrow 1$	$Ee^{3+}+3e$	(anode)	(2)
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$\rm 2H_2O + 2e \rightarrow$	$H_2 + 2OH^-$	(cathode)	(3)
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 $Fe^{2+}+2OH^{-} \rightarrow Fe(OH)_{2}$ (coagulant) (4)

$$Fe^{3+}+ 3OH^{-} \rightarrow Fe(OH)_{3}$$
 (coagulant) (5)

B) Aluminum electrodes:

 $Al \rightarrow Al^{3+} + 3e$ (anode) (6)

 $2H_2O + 2e \rightarrow H_2 + 2OH$ (cathode) (7)

$$Al^{3+}+ 3OH^{-} \rightarrow Al(OH)_{3}$$
 (coagulant) (8)

The produced metallic cations  $Fe^{2+}$ ,  $Fe^{3+}$  and  $Al^{3+}$  from the corresponding anodic reactions (1), (2) and (6) induce a reduction of the colloidal matter's net surface charge resulting in destabilization followed by coagulation. Furthermore, Fe<sup>2+</sup>, Fe<sup>3+</sup> and Al<sup>3+</sup> cations combine with the cathodically generated OH anions according to the reactions (4), (5) and (8) to form the known coagulant precipitates, Fe(OH)<sub>2</sub>, Fe(OH)<sub>3</sub>and Al(OH)<sub>3</sub> that are capable of adsorbing both organic and inorganic pollutants [12,13]. Simultaneously hydrogen gas bubbles are generated at the cathode contributing to the flotation of particulate matter and flocs. The sludge formed can be further separated from the treated solution either by filtration or centrifugation. Based on the

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above, the electrocoagulation removal of pollutants may involve mechanisms such as oxidation, reduction, coagulation, absorption, flotation, and precipitation[14,15].

The present study aimed to evaluate the electrocoagulation process for high-salinity landfill-leachate processing. The study focused on the effect of electrode type, the applied current density, processing time and pH, in relation to the removal of ammonia and COD. Finally a comparison with similar studies reported in the literature was performed.

#### 2. Material and Methods

#### 2.1. Leachate and reagents

The leachate samples used for this study were obtained from a sanitary landfill located in North Greece. The site was in operation since 2005and received both municipal, industrial, and agro-industrial wastes and sludges. The reagents used for pH adjustment (HCl, NaOH) were all of analytical grade (Merck).

#### 2.2. Experimental design and apparatus

Electrocoagulation experiments were conducted at room temperature using a cylindrical electrochemical reactor (250 mL working volume) equipped with a magnetic stirrer (Thermodyne, Nuova II Stir Plate), operated at 300 rpm. Two commercially iron (St 37-2 steel) (according to German standard DIN 17100) or aluminum plates (2024 aluminum alloy) were used as electrodes with size  $8 \times 5 \times 0.3$  cm and an effective area of 25 cm<sup>2</sup> each. The electrodes were placed vertically parallel to each other, having an inter-electrode distance of 1cm. The electrodes were connected to a DC power supply (STELLTRAFO, PHYWE SystemeGmbh&Co, Germany) to provide constant current and a multimeter (VOLTCRAFT 91) measuring electron potential and current.

The efficiency of the electrocoagulation treatment during landfill leachate processing was studied for different current densities (12, 24, and 36 mA cm<sup>-2</sup>), electro-processing time (50, 100, 150, 200, and 240 min), type of electrodes (iron and aluminum) and various initial solution pH values. Every 50 minutes of electro-processing time, liquid samples were extracted from the reactor medium, filtered with whatman paper, and analyzed for pH, electrical conductivity, chemical oxygen demand (COD), and ammonia nitrogen (NH<sub>4</sub>-N). COD measurements were performed using a COD thermoreactor (Tr 420, Merk) and a spectrophotometer (Spectroquant Pharo100, Merk), according to the Standard Methods for examination of water and wastewater.

#### 3. Results and discussion

#### 3.1. Landfill-leachate characteristics

The main characteristics of the landfill-leachate used for this study are shown in Table 1. The BOD/COD ratio was equal to 0.15, indicating that the landfill was old; besides, it is in operation for more than 15 years. Similar leachate composition was recorded in municipal solid waste landfills in Brazil, India and Malaysia (see Table 1). Based on the results from Table 1 landfill leachate electrical conductivity may vary from 5 up to 35 mS cm<sup>-1</sup>. In our case, the leachate's high electrical conductivity was attributed to the implementation of reverse osmosis for leachate processing, where the generated concentrates were continuously recirculated back onto the landfill body. In a similar case study, a significant increase of the leachate chlorides concentration from 2.18 to 3.52 g L<sup>-1</sup>was observed after implementing reverse osmosis with recirculation of the concentrates onto the landfill body [16].

Londfill site	Creases	Canada	China	Malaysia	Dragil	India	
leachate used for this study indicate the standard deviation (n=10).							
Table 1. Physicochemica	al properties of landfill-le	eachate from dif	ferent origin.	The numbers in	n parenthesis fo	or the landfill	

Landfill site	Greece	Canada	China	Malaysia	Brazil	India
Waste origin	MSW+ISW+SS	MSW	nr	MSW	MSW	nr
Commissioning	2005	2000	2005	2005	2007	2013
рН (-)	7.54 (±0.35)	7.83	nr	8.17	7.90	8.64
EC (mS cm <sup>-1</sup> )	25.8 (±1.9)	5.29	nr	29.2	7.94	36.5
<b>BOD</b> (mg $L^{-1}$ )	1300 (±880)	460	960	540	923	1519
$COD (mg L^{-1})$	8870 (±1360)	1620	2566	10000	4200	13760
NH <sub>4</sub> -N (mg L <sup>-1</sup> )	872 (±200)	653	386	5800	1648	nr
References	This study	[6]	[7]	[8]	[9]	[10]

MSW - municipal solid waste, ISW - industrial solid waste, SS - sewage sludge, nr - not reported

## **3.2.** Effect of reaction time and applied current density on COD removal

Figure 1 demonstrates the effect of processing time on COD removal efficiency using iron or aluminum electrodes. For iron electrodes the data reveal that COD removal increased with the applied electro-processing time and with increasing current density. Indeed, maximum COD removal (78.5%) was recorded after 240, 140, and 90 min processing time with increasing current density from 12 to 24 and 36 mA cm<sup>-2</sup> respectively. Similar COD removal (60%) was reported in the literature using iron electrodes at 180 min processing time and 30 mA cm<sup>-2</sup> current density [17]. Current density affects the rate of coagulants' release (by the anode) and hydrogen gas production (by the cathode). The latter can adsorb to

particulate and flocculent matter, causing flotation. A study conducted at low current density (3 mA cm<sup>-2</sup>) resulted in a COD removal of 33% after 50 min [18] while at a current density of 16 mA cm<sup>-2</sup>, COD removal was 40% after 90 min of electrocoagulation time [19], which is comparable with the results of this work. The current density increases the electron's flow velocity due to ions' electrostatic attraction through the oppositely charged electrodes, further increasing the coagulant flocs (sludge) increased from 16 to 60% (v/v) with increasing current density from 12 and 40 mA cm<sup>-2</sup>.

For aluminum electrodes, COD removal efficiency increased with the applied current density (see Figure 1b). In

this case, maximum COD removal (72.5%) was recorded after 240, 140, and 90 min processing time, at an applied current density of 12, 24 and 36 mA cm<sup>-2</sup>, respectively. As evidenced by the results presented therein, up to 72% COD removal is possible within 240 min processing time. Based on previous studies, landfill leachate COD removal efficiency increased from 40 to 60 and 65% using aluminum electrodes, with increasing current density from 16 to 38 and 50 mA cm<sup>-2</sup> respectively, which is within the same range with the results of this work.

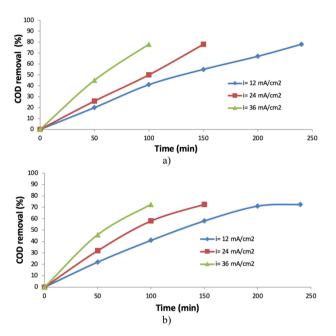


Fig. 1. COD removal efficiency as a function of time at various current densities for landfill leachate electrocoagulation with a) iron and b) aluminum electrodes.

The time required to achieve the desired removal efficiency is essential for the design of an electrochemical treatment technology. The electrocoagulation process is separated into two phases, coagulation (destabilization of charged colloidal particles) and flocculation (aggregation of colloids), with the first being accomplished within a short time period (usually between 5 and 10 min depending on the rate of coagulant release) and the second between 20-50 min depending on the mixing conditions inside the reactor [15, 21]. The Fe<sup>2+</sup>, Fe<sup>3+</sup> and Al<sup>3+</sup>ions released by electrodissolution of the anodes are well known to decrease colloids' net surface charge. A short operating time results in low charge neutralization, and the produced metal ions are not enough to destabilize the colloids. Therefore, increasing processing time is generally related to higher COD removal since more iron or aluminum cations are released, which act as the coagulant. Moreover, flotation of the precipitates and flocs formed occurs by the generated hydrogen gas bubbles, resulting in additional separation of the organics [7, 22, 23]. As shown in the data provided in Table 2, the implementation of iron or aluminum electrodes resulted in a significant increase of the solution electrical conductivity. This was attributed to the release of coagulants. According to Bouhezila et al[20] iron electrodes were more efficient than aluminum electrodesto remove COD under the same operating conditions, which is consistent with the results of this work. Also, iron is less toxic and acceptable in case that the treated effluent is reusedin agriculture.

#### 3.3. Effect of initial pH

As observed in previous studies, the solution's initial pH is a critical factor influencing the efficiency of the electrocoagulation process (e.g. [18,19]). According to the data presented in Table 3 (for iron electrodes), it becomes evident that the leachate solution's pH increases during the electrochemical treatment. Galvao et al [19] reported a similar pH increase from 7.9 to 9.0 during electrocoagulation of landfill leachate at 13 mA cm<sup>-2</sup> and 90 min processing time. Other studies showed that for initial pH values between 4 and 7, the observed increase of solution pH was attributed to the generation of OH- ions at the cathode [24, 25].

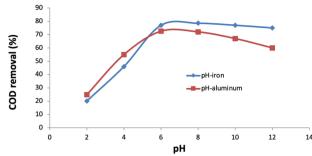
**Table 2.** Evolution of the electrical conductivity (EC), temperature and COD during landfill-leachate processing with iron or aluminum electrodes at a current density  $36 \text{ mA} \text{ cm}^{-2}$ .

Time (min) EC (mScm <sup>-1</sup> )		T (°C)	COD(mgL <sup>-1</sup> )					
Iron electrodes								
0	25,8	28	9890					
50	26,5	29	4850					
100	26,9	30	2130					
150	27,8	30.6	1580					
200	28,2	32	1167					
240	30,4	33	927					
	Aluminum electrodes							
0	25,8	28	9890					
50	30,6	34	5440					
100	31,2	37	2715					
150	32,1	38	2374					
200	32,4	39	2067					
240	32,5	39,5	1854					

According to Figure 2, the optimal initial pH was recorded between 6 and 8, where the coagulants' hydroxide form Fe(OH)<sub>2</sub>, Fe(OH)<sub>3</sub> and Al(OH)<sub>3</sub> prevails. This is within the range of typical leachate samples (see Table 1). At pH<3 (acidic conditions) and pH >9 (basic conditions), the corresponding cationic form, Fe<sup>2+</sup>, Fe<sup>3+</sup> Al<sup>3+</sup> and a series of polymeric anionic forms, especially for aluminum, are predominant, which do not favor the coagulation process. Under acidic conditions, the removal efficiency of aluminum is equal or even better compared to iron, due to enhanced tendency for production of more Fe<sup>2+</sup> than Fe<sup>3+</sup> ions. Indeed, ferrous ions are weaker coagulants compared to ferric ions.Similar to our results, Li et al [18]and Le et al [26]observed that the optimum pH conditions for landfill leachate electrocoagulation was between 6 and 8 using iron or aluminum electrodes.

**Table 3.** Evolution of pH and COD removalas a function of time for landfill leachate electrocoagulation with iron electrodes at 12 mA cm<sup>-2</sup>current density.

Processing time	pН	CODRemoval
(min)		(%)
0	7.54	0
50	8.64	22
100	8.86	40
150	9.15	56
200	9.43	73
240	9.52	78.5



**Fig. 2.** Effect of solution pH on COD removal efficiency for landfill leachate electrocoagulation with iron and aluminum electrodes at  $12 \text{ mA} \text{ cm}^{-2}$  current density and 240 min processing time.

# 3.4. Effect of reaction time,type of electrodes and applied current density on NH<sub>4</sub>-N removal

Figure 3 shows that increasing current density was beneficial for NH<sub>4</sub>-N removal. Considering the treatment conditions applied in this study (pH = 7.54, and reaction time 240 min), iron electrodes were more effective than aluminum for NH<sub>4</sub>-N removal. Indeed, after 240 min of electro-processing time at 12 mA cm<sup>-2</sup> current density, maximum NH<sub>4</sub>-N removal efficiency was 62% and 54% for iron and aluminum electrodes, respectively. Based on the results from previous studies, ammonia nitrogen removal efficiency ranged between 6 and 50% (see Table 4). Most of these studies, however, were conducted at low electro-processing time (often less than 60 min). The removal of ammonia is generally attributed to the increase in solution pH, which in turns favor ammonia stripping by the generated hydrogen bubbles.

 Table 4. Comparison of NH4-N removal efficiency during landfill leachate electrocoagulation using iron or aluminum electrodes at different processing times and current densities.

Leachate		Equ	ıipment	Conditions		Removal	
NH <sub>4</sub> -N	pH (-)	Anode	Cathode	Time	Current	NH <sub>4</sub> -N	References
(mg/L)		material	material	(min)	(mA cm <sup>-2</sup> )	(%)	
653	7.83	Aluminum	Stainless steel	30	15	6	[27]
1615	8.25	Aluminum	Aluminum	30	50	15	[20]
386	6.85	Aluminum	Aluminum	50	3	24	[18]
216	8.24	Aluminum	Aluminum	60	38	40	[28]
980	8.30	Aluminum	Aluminum	120	50	30	[10]
872	7.54	Aluminum	Aluminum	240	36	54	This study
1615	8.25	Iron	Iron	30	50	24	[20]
386	6.85	Iron	Iron	50	3	28	[18]
1256	8.00	Iron	Stainless steel	60	0.4	27	[26]
3000	6.50	Iron	Aluminum	60	56	50	[29]
872	7.54	Iron	Iron	240	36	62	This study

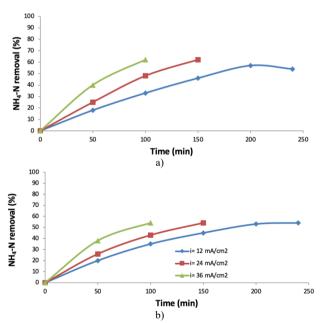


Fig. 3. Effect of current density and processing time on NH<sub>4</sub>-N removal efficiency for landfill leachate electrocoagulation with a) iron and b) aluminum electrodes.

#### 4. Conclusions

This study indicates that the electrocoagulation process was efficient for COD and ammonia nitrogen removal from a high-salinity landfill-leachate. The experimental results showed that the treatment efficiency increases proportionally with increasing the applied current density and reaction time. Furthermore, it was found that iron electrodes were more effective compared to aluminum electrodes, especially at higher applied current density. Compared to similar studies it was observed that ammonia nitrogen removal is favored at high electro-processing times. Electrocoagulation consist an interesting technology for pollutants removal from leachates. Future studies should focus on field-scale applications to further evaluate long term efficiency and the costs involved.

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