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Nuclear Magnetic Resonance and Acoustic Emission on Initial Crack and Fracture Development of Coal with Different Strengths

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Abstract

The initial fracture and development of fracture under loading conditions of coal are closely related to the stability of surrounding rock and geo-dynamic disasters. In this study, nuclear magnetic resonance (NMR), acoustic emission (AE) and 3D-CAD reduction techniques were employed to analyze the initial fracture distribution, the fracture development and failure mode of coal samples with different strengths under uniaxial loading. Based on NMR and 3D-CAD reduction, the initial fracture rate and fracture distribution of coal samples were obtained. Through uniaxial loading and AE, the distribution of fracture points was analysed. The dominated fracture of the failure state was reconstructed using 3D-CAD. Results show the initial crack rate of hard coal is low, and the ringing accounts and AE energy are small in the initial stage of loading. However, they increase rapidly in the later stage of loading, showing the characteristics of brittleness. In the initial state, the fracture rate of soft coal sample is higher than that of hard coal, and the growth of fracture point is fast. In the later stage, the fracture point number and AE energy are similar to that of hard coal. The initial fracture rate and fracture similar fracture strengths are different, resulting in different occurrence and development of secondary fractures in loading state, which indicates that the deformational behaviour, failure mode and energy release are different for coal with different strengths. This study provides a theoretical basis for the stability analysis and geo-dynamic disasters prevention of coal with different strengths.

Keywords: Coal, Crack, Fracture, Energy, Acoustic emission

1. Introduction

From the perspective of mining engineering, the structural instability of coal and rock mass and geological dynamic disasters such as rockburst are closely related to the bearing capacity, failure mode and energy accumulation within the coal mass. As coal is a discontinuous medium composed by matrix and fractures, the distribution of the primary cracks and the fracture development under loading conditions are the keys for the failure characteristics and energy evolution of the coal mass [1]. Therefore, it is of great significance to study the distribution of initial coal cracks and the fracture development for the stability of surrounding rock and the prevention of geo-disasters.

Nuclear magnetic resonance (NMR) technology is a physical process in which the nuclear spin energy levels are Zeeman separated by an external magnetic field on the atomic nucleus with non-zero nuclear magnetic moment, and the RF radiation of a specific frequency is absorbed by resonance. At present, NMR technology is used in the rock mechanics to test the hydrogen atoms in rock fractures to obtain the distribution of internal fractures [2]. NMR does not damage the structure of rock, so, Mechanical tests can be conducted after NMR testing.

Acoustic emission (AE) technology is a method to obtain the damage and crack position in materials based on the emission and detection of elastic waves. AE technology

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can accurately determine the damage position of materials in the process of dynamic loading. The AE testing can also measure the energy change of the sample in the loading process. In recent years, as a non-destructive testing technology, AE is widely used in the field of mining engineering [3-4].

Based on the characteristics and advantages of the above technologies, this study selects coal samples with different strengths, uses NMR technology to measure the initial cracks in coal samples to study the crack distribution and crack rate within the coal samples. Then, AE technology is used to detect the fracture development in the process of rock failure. By analyzing the ringing distribution and AE energy in the loading process, the crack development and failure mode are obtained. In addition, the key fracture that dominates the deformation and failure of the coal sample are restored by 3D-CAD. The distribution and development of coal fractures were studied by using NMR, AE and 3D-CAD restore technology, which provides a theoretical basis and testing method for the study of bearing characteristics, failure occurrence and energy accumulation of coal with different strengths.

2. State of the art

The macro-fracture of coal is important in its bearing capacity and failure mode. In the 1920s, it was found that the cracks changed its internal stress state, and the cracks could expand and penetrate under loading, resulting in material damage [5]. Hoek-Brown criterion was used to measure the

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strength of rock mass with cracks, and provides a method for the relationship between rock mass strength and cracks [6]. Ingraffea et al. studied the expansion of cracks and its influence on rock strength through uniaxial compression test. They proposed that the increase and penetration of internal cracks in rock samples are the reason for the final failure of rock [7-8]. Wang et al. prepared samples of the similar materials and prefabricated cracks, and conducted the seepage behaviour of fractured rock mass infilling using different transfixion rates under cyclic loading [9].

With regard to the research on the relationship between structure failure and dynamic disasters, Pan et al. analyzed the energy storage and energy consumption of coal and rock from the perspective of micro-structure and constructed a quantitative relationship between the lithologic fabric of the coal and rock mass and its impact tendency [10]. Zhao et al. used X-ray diffraction, SEM and automatic micro photometer to analyze the strength of coal impact tendency, and obtained the relationship between coal internal mesostructure parameters and impact tendency [11]. Jiang et al. used XRD, paramagnetic resonance, SEM to obtain the structural differences of coal and rock samples before and after rockburst, and explored the characteristics of energy dissipation in the process of rockburst incubation and occurrence [12]. Xue et al. found that the fractal reconstruction could describe the anisotropy effectively and the four roughness descriptors of asperity height, inclination angle, line length and surface area descriptors showed high precision for fractal dimension calculation [13]. In fact, coal is a typical soft rock, whereas its deformational behaviour is dominated by the two aspects: micro-structure and gas migration [14]. The structure of coal and rock is contributed to its geological conditions, including cleats and joints generated before and after formation of the coal and rock [15-19]. However, there are few studies on the influence of initial joint and fracture development on the deformation and failure characteristics and energy accumulation of coal and rock mass [20-23].

Therefore, this study will study the failure mode, strength and energy accumulation of coal and rock mass from the perspective of internal crack and fracture of coal and rock mass with different bearing capacity, and explore the essential relationship between deformation and failure and energy accumulation of the coal with different strengths to understand the mechanism of coal deformation and dynamic disasters in coal mines from the aspect of joints and fissures.

The rest of this study is organized as follows. Section 3 describes the samples and tesing procedure. Section 4 gives the experimental results and discussion. Finally, the conclusions are summarized in Section 5.

3. Methodology

3.1 Sample preparation

The testing samples are taken from Datong Xinzhouyao coal mine and Shuangya coal mine. The average compressive strength of the coal samples from Xinzhouyao coal mine is 30 MPa and the average compressive strength of the coal samples from Dongrong No. 2 coal mine is 10 MPa. Two kinds of coal samples with different strengths are selected in the test to compare and contrast the influence of initial cracks, the deformation characteristics, failure modes and energy accumulation characteristics of coal.

After the coal sample was taken, it was processed by rock cutter and coring machine to $\phi 50 \text{ mm} \times 100 \text{ mm}$ standard rock mechanics testing specimen. The cross-section parallelism was controlled within $\pm 0.02 \text{ mm}$. A total of 18 samples are prepared, 9 samples from each coal mine, as shown in Fig. 1. After the sample was prepared, it was distinguished according to the surface cracks, then the samples are scanned by NMR imaging technology to obtain the spatial distribution of cracks in the samples, and finally they are grouped according to different cracks.



Fig. 1. Coal samples used in this study.

3.2 NMR testing

The NMR equipment is shown in Fig. 2(a). The applied intensity of the magnetic field is 0.3-0.5 T, the main frequency of the instrument is 12 MHz. To ensure that the sample is in the middle of the magnetic field, the coil diameter of the magnetic field was selected as 60 mm. As shown in Fig. 2(b), the analysis equipment is a nuclear magnetic imaging software and a gradient pulse instrument. The imaging software can set the slice width, number of slices and slice gap of the sample. After positioning, prescanning, formal scanning and imaging of the sample, the crack structure inside the sample is displayed in the form of slices.



(a) NMR cell (b) NMR processing unit Fig. 2. NMR equipment used in this study

The internal fracture distribution map of the sample can be obtained by processing the three-dimensional slice map using NMR 3D reconstruction software. The NMR 3D reconstruction map of typical samples in Xinzhouyao coal mine is shown in Fig. 3, in which the white areas indicate the fracture.



(a) Main view (b) Top view (c) Side view Fig. 3. NMR reconstruction of Xinzhouyao coal mine samples



Fig. 4. Basic composition of acoustic emission system.

3.3 Experimental Procedure

WAW-600C computer-aided electro-hydraulic servo universal testing machine is used to conduct the compressive test. AE monitoring device is instrumented to observe the dynamic response of the specimen structure under uniaxial loading. The maximum loading capability is 600 kN, the maximum laoding velocity is 70 mm/min and the maximum distance between the compression plates is 500 mm.

The uniaxial compression testing system and the AE monitoring system are used to dynamically monitor the experimental data. The uniaxial compression testing machine is controlled by displacement with a loading rate of 0.5 mm/min. For parameters of the AE instrument, the threshold of the AE monitoring is set as 45 dB to minimize the effect of surrounding noises. The peak definition time (PDT), the hit definition time (HDT), and the hit locking time (HLT) are selected as 300 µs, 600 µs, and 1000 µs, respectively. The sound velocity is set to be 1.8 km/s.

After parameter setting was completed, fusing test was conducted on the specimen to verify the sensitivity of each sensor to guarantee the reliability of the experiment. After the parameter setting and fusing testing are completed, uniaxial compression tests are carried out. The stress loading system and the AE monitoring system were turned on simultaneously. The experimental arrangement and the posttesting samples are shown in Fig. 5.



Fig. 5. Before and after testing samples

3.4 AE testing

The AE technology is an effective method to detect the dynamic change of the material structure under the action of external loading through instrumentation. Each channel of the data acquisition system consists of measuring instrument, digital signal processor, computation program and other peripheral apparatus, which are finally connected to a computer. The components of each channel include an AE sensor, a preamplifier, and a data acquisition card, as shown in Fig. 4.



4. Results and Discussion

4.1 The initial crack rate and distribution

According to the NMR data, the initial crack rate can be calculated. As the internal crack of the sample is an irregular body, to simply the calculation, the internal crack of the sample is regarded as a regular cuboid, and the parameter index is length, width and height. Table 1 shows the specific parameters of the internal crack of the coal samples. The sample number of Xinzhouyao coal mine starts with X and that of Dongrong No. 2 coal mine starts with D. the crack rate of the coal sample is calculated, as shown in Table 2.

By import the 3D slice diagram of the sample into CAD, the CAD 3D reconstruction diagram shows the fracture development and parameters. The CAD three-dimensional reconstruction diagram is shown in the Fig. 6.

4.2 Crack development and distribution

The AE detection threshold was set to 45 dB and the sound speed is 1.8 km / s. Fig. 7 shows the representative AE fracture point of coal sample and the corresponding CAD reconstruction diagram.

It can be seen that the original fracture exists at the first position of the fracture point. With the progress of loading, the original fracture begins to expand and penetrate until the sample is damaged. During this period, the AE fracture point increases with the fracture, and the positions of fracture points are the positions of fracture expansion. Comparing X1 and X2, in which X1 fracture rate is 0.06% and X2 fracture rate is 0.18%, it can be seen that the higher the fracture rate is, the earlier the fracture point appears. Comparing X2 sample with different strengths with D2, X2 fracture rate is 0.18%, D2 fracture rate is 0.17%, and the difference of fracture rate is only 0.01%, which can be ignored. However, the occurrence time of X2 fracture point of sample is 3 times that of D2 fracture point. Therefore, the greater the strength, the later the occurrence time of fracture point of sample. From the simple analysis of the total stress-strain curve of uniaxial compression, the stage of fracture points is the compaction stage, and the time stage of a large number of fracture points is the middle stage of linear elasticity stage.

			Dimension			
Name	No.	Position	Direction	Length (mm)	Width (mm)	Thickness (mm)
X1-1	1	Top 5.2mm	Horizontal	23.8	13.2	0.25
X1-2	1	Bottom 12.3mm	Horizontal 30°	25.8	9.5	0.96
3/1 0	1	Bottom 38 mm	Horizontal 45°	27.6	13.8	0.62
X1-3	2	inclined	Vertical	25.3	19.3	0.78
X2-1	1	Bottom 5 mm	Horizontal	19.2	17	0.36
X2-2	1	Top 45 mm	Horizontal	33.1	16.4	0.40
	2	Тор	Vertical	24.3	13.2	0.42
	1	Top 55 mm	Horizontal	19.5	17.9	1.00
X2-3	2	Top 50 mm	Horizontal	27.4	16.3	0.3
	3	Top 10mm	Vertical	21.3	10.1	0.22
X3-1	1	Top-middle	Vertical	38.3	15.3	0.1
V2 2	1	Top-middle	Vertical	48.3	9.3	0.3
A3-2	2	Middle	Horizontal 80°	30.1	18.2	0.25
	1	Bottom 10mm	Horizontal	26.3	16.1	0.5
X3-3	2	Bottom 20mm	Horizontal	28.4	15.0	0.5
	3	Bottom 35mm	Horizontal	23.4	21.5	0.52
D1-1	1	Bottom 20mm	Horizontal 60°	42.3	8.4	0.55
D1 2	1	Middle-bottom	Vertical	38.7	10.0	0.77
D1-2	2	Bottom 40mm	Horizontal 45°	23.6	13.1	0.68
	1	Bottom 45mm	Horizontal	24.7	17.6	0.40
D1 2	2	Bottom	Horizontal 60°	41.7	18.2	0.32
D1-5	3	Тор	Vertical	38.0	21.4	0.41
	4	Тор	Vertical	46.8	13.9	0.60
D2-1	1	Bottom 46mm	Horizontal	35.2	18.3	0.52
D2 2	1	Bottom 33mm	Horizontal 30°	22.0	18.2	1.13
D2-2	2	Тор	Vertical	42.3	7.2	0.71
	1	Bottom 27mm	Vertical	22.5	17.8	0.63
D2-3	2	Bottom	Horizontal 50°	32.3	28.7	0.69
	3	Тор	Vertical	26.5	22.5	0.4
D3-1	1	Top 30mm	Horizontal	27.4	19.8	0.48
	2	Bottom 42mm	Horizontal 55°	24.1	18.4	0.63
D3-2	1	Bottom	Vertical	50.0	17.0	0.42
	2	Bottom 24mm	Horizontal 40°	23.4	21.4	0.73
	3	Тор	Vertical	52.0	23.8	0.31
D3-3	1	Bottom 13mm	Horizontal 60°	64.7	15.2	1.2
	2	Bottom	Vertical	51.3	22.4	0.28
	3	Top 15mm	Horizontal	18.4	16.7	0.4
	4	Top 17mm	Vertical	23.4	8.4	0.23

Table. 1	The initial	crack of	each coal	sample

Table. 2 Basic information and fracture rate of coal samples

Name	No.	Dimen	Creaty note	
		Diameter (mm)	Height (mm)	Crack rate
х	X1-1	50.14	100.84	0.04%
	X1-2	50.21	100.10	0.12%
	X1-3	50.11	100.03	0.32%
	X2-1	50.17	100.05	0.06%
	X2-2	50.12	100.63	0.18%
	X2-3	50.08	100.42	0.27%
	X3-1	50.04	100.04	0.03%
	X3-2	50.17	100.84	0.14%
	X3-3	50.02	100.45	0.35%
D	D1-1	50.08	100.51	0.10%
	D1-2	50.10	100.08	0.26%
	D1-3	50.03	100.77	0.58%
	D2-1	50.07	100.25	0.17%
	D2-2	50.13	100.15	0.33%
	D2-3	50.05	100.51	0.58%
	D3-1	50.04	100.45	0.28%
	D3-2	50.13	100.09	0.55%
	D3-3	50.08	100.11	0.84%



Fig. 6. CAD 3D reconstruction diagrams of X and D samples.





Fig. 7. AE fracture point and the corresponding CAD reconstruction diagrams of X1, X2, D1, and D2.

4.3 Ring accounts and uniaxial strength

By processing the AE data, the ring account and stress and energy diagram of each sample are obtained. The stress is obtained from the uniaxial compression data, and the ringing count and energy are detected by the AE instrument. Typical diagram is shown in Fig. 8.







Fig. 8. Ring accounts and energy of AE of X1, X2, X3, D1, D2, and D3.

The ringing count in the is the number of times that the shock wave generated when the sample is over the detection threshold. The more the ringing count, the more the internal damage of the sample. The energy diagram is not the real energy released by the specimen damage, but the AE records the output in the form of corresponding energy value.

X1 sample with the smallest crack number and crack rate has almost no ring count within 360 s at the initial stage of loading. After that, the ring count increases slowly until the ring count suddenly rises straight in the linear elastic stage, and the total number reaches 8.2×106 times. The ring count of X2 sample with relatively large crack number and crack rate is very similar to that of X3 sample, which is relatively gentle compared with X1 sample, and the ring count reaches 5.1×106 times and 6.5×106 times. As there are many primary cracks in X2 and X3 samples, so the failure mode of them is slow expansion and penetration of multiple cracks until failure. The X1 sample has fewer internal cracks, therefore, the failure of the sample is the sudden occurred, and the ring count shows a trend of slowly increasing to straight rising.

The stress energy diagram of X samples shows that, the energy curve trend of X1 sample with low fracture rate is consistent with its ring count trend. It also shows a straight rise from the slow increase in the initial stage of loading to the linear elastic stage, which is consistent with the failure characteristics of less cracks in the sample, resulting in secondary cracks and rapid expansion. The final energy peak is 4.8×1010 J/s. The energy curve trend of X2 and X3 samples with high fracture rate is also consistent with their failure characteristics. They show the trend that the energy value increases slowly in the initial stage of loading until a small increase in the linear elastic stage, and their energy peaks are 3.8×1010 and 3.1×1010 J/s, respectively.

The average compressive strength of the D sample is only 10 MPa. The coal is soft and the fracture rate is higher than that of X. Therefore, the law of ring count curve and energy value curve is different from that of X. The ring counts of the three samples appear at the initial stage of stress loading, and the ring counts gradually increase with the progress of loading, and the ring counts are 1.2×105 , 3.1×106 and 4.0×106 respectively. It can be seen that the failure characteristics of coal samples with more cracks are the joint expansion and penetration of multiple cracks in the sample and the slow increase of secondary cracks until the sample is damaged. In terms of stress energy diagram, D1 sample with the lowest crack rate has no energy value at the initial stage of loading, and the energy value increases slightly at the online elastic stage, with a peak value of $3.0 \times$ 1010 J / s. D2 and D3 samples with high fracture rate have energy values from the initial stage of stress loading, and then gradually increase, with peak values of 3.8× 1010 and 3.3×1010 J/s, respectively.

4.4 Failure process of fractured coal mass

Through the analysis of the NMR and AE test results of coal samples in, it can be seen that the crack is the main factor affecting the failure characteristics and energy accumulation for coal samples. The ring count and energy peak stage of coal samples are statistically analyzed, as shown in Table 3.

Table.	3 Failure	proces
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Table. 5 Tallule process				1
Name	No.	Crack	Ring account	Peak energy
	X1-1	0.04%	Ealy elastic	Later elastic
	X1-2	0.12%	Later compaction	Later elastic
	X1-3	0.32%	Ealy compaction	Ealy elastic
	X2-1	0.06%	Middle elastic	Peak
Х	X2-2	0.18%	Later compaction	Later elastic
	X2-3	0.27%	Later compaction	Ealy elastic
	X3-1 0.03% Middle compaction		Peak	
	X3-2 0.14% Middle compaction		Peak	
	X3-3	0.35%	Ealy compaction	Later elastic
	S1-1	0.10%	Ealy compaction	Later elastic
	S1-2	0.26%	Ealy compaction	Residual
	S1-3	0.58%	Ealy compaction	Later
	S2-1	0.17%	Middle elastic	Later elastic
D	S2-2	0.33%	Later compaction	Peak
	S2-3	0.58%	Ealy compaction	Ealy compaction
	S3-1	0.28%	Ealy elastic	Peak
	S3-2	0.55%	Later compaction	Later elastic
	S3-3	0.84%	Ealy compaction	Middle elastic

As shown in Table 3, due to the different fracture rates of each coal sample, the ring count and energy peak are also different. It can be seen from the analysis that the internal cracks of the sample increase with the loading, and the stages of ring count and energy peak are different. On the other hand, due to the increase of cracks in the sample, the accumulated energy of the sample is released in advance, and the time of energy accumulation of the sample becomes shorter.

5. Conclusions

In this study, from the point of view of the initial cracks distribution and crack rate of the sample, the influence of the fracture development of the coal sample with different on the failure characteristics and energy accumulation is studied using NMR, EA and CAD-3D restoration technologies. Following conclusions can be obtained:

(1) The number of cracks and its parameters in coal samples are quantified by measurement and calculation by the NMR imaging technology and CAD-3D reconstruction, which are dominated factors for fracture development under loading conditions;

(2) Through the uniaxial compression test, acoustic emission properties are obtained to study the failure mode of coal samples with different fracture rate. Results shows that sample with high compressive strength are manifested in the expansion and penetration of the internal primary fractures; and that of the sample with low compressive strength derived secondary fractures, for which, the ring count curve shows a slow upward trend; (3) The failure mode of samples with low fracture rate are that with the gradual loading to the linear elastic stage, a large number of secondary fractures are rapidly derived from the existing primary fractures, so that the ring count curve suddenly rises straight from the linear elastic stage;

(4) In terms of AE energy accumulation, by drawing the curves of fracture number, fracture rate and energy peak, it is concluded that the energy of samples with higher fracture number and fracture rate is released in advance and the energy peak is reduced.

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